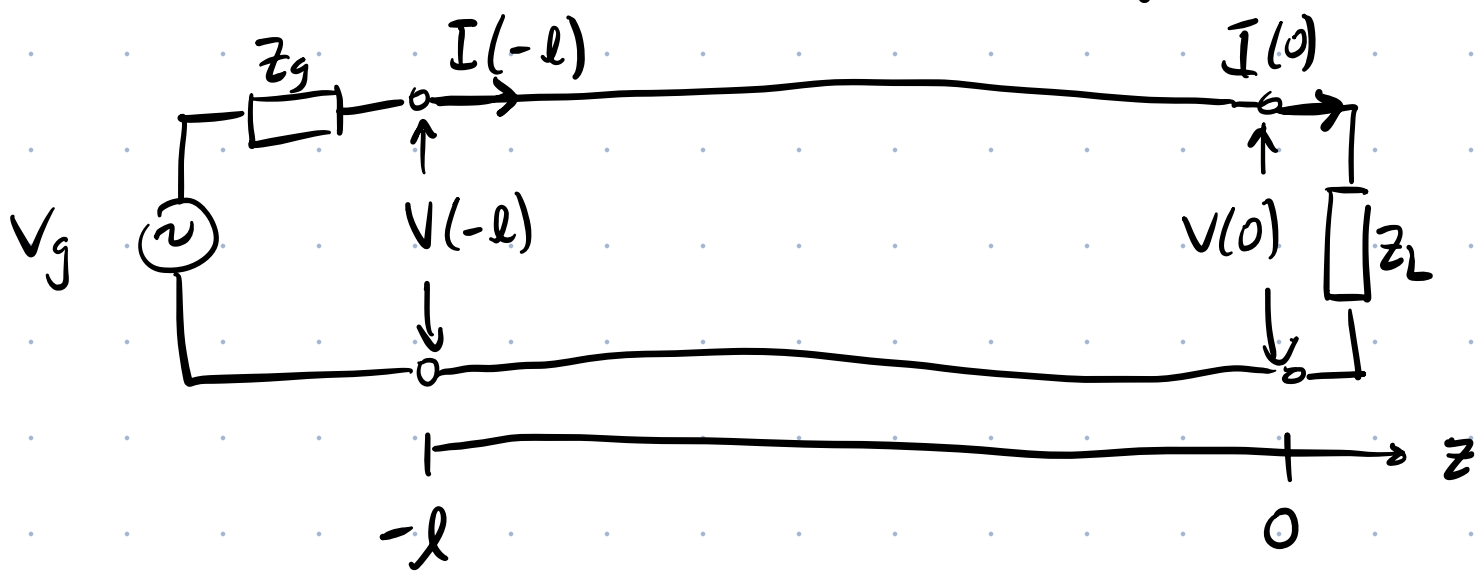


Useful results from earlier in the term:

- Transmission line results for amplitude of harmonic voltage & current



Frequency Domain

$$\begin{cases}
 V(z, \omega) = V_+ [e^{-j\beta z} + \Gamma e^{j\beta z}] \equiv \hat{V}(z, \omega) \\
 I(z, \omega) = \frac{V_+}{Z_0} [e^{-j\beta z} - \Gamma e^{j\beta z}] \equiv \hat{I}(z, \omega)
 \end{cases}$$

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$$

$$\beta = \omega \sqrt{L_l C_l} = \frac{\omega}{s}$$

prop. speed.

② Inverse Fourier Transforms

$$(a) f(t) = F^{-1}[\hat{f}(\omega)] = \frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{f}(\omega) e^{j\omega t} d\omega$$

$$(b) \text{ Delta fun: } \delta(t-t_0) = \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{j\omega(t-t_0)} d\omega$$

(c) Convolution Theorem

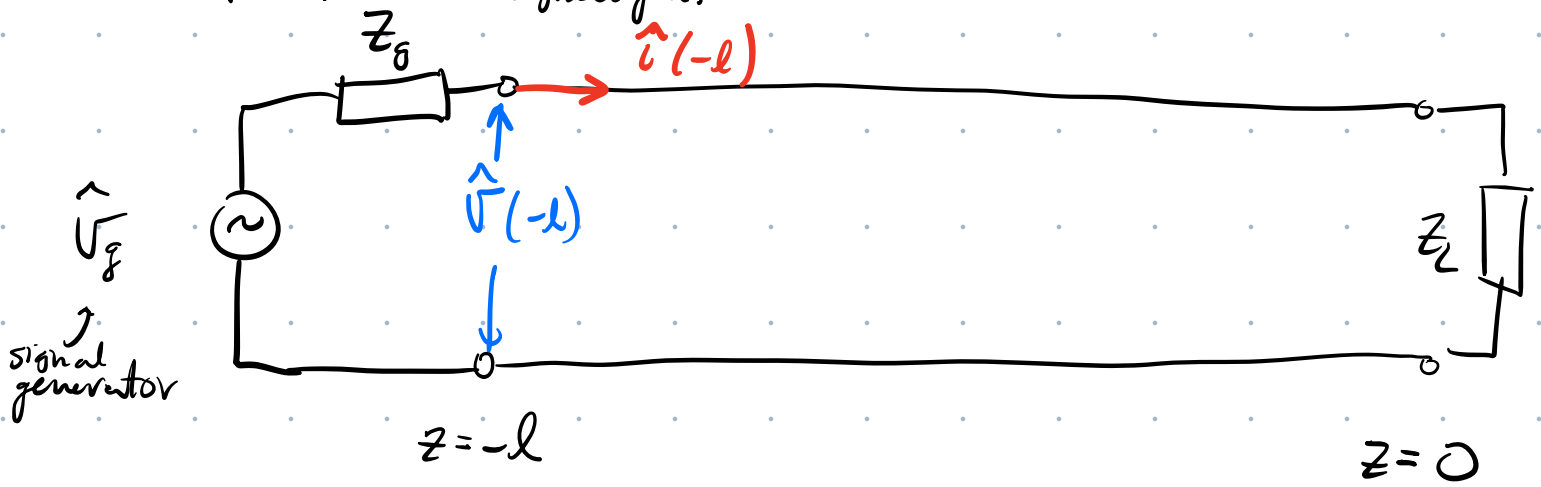
$$F^{-1}[\hat{x}_1(\omega) \hat{x}_2(\omega)] = x_1(t) * x_2(t) \\ = \int_{-\infty}^{\infty} x_1(\tau) x_2(t-\tau) d\tau$$

Goal is to calc. transient response (time domain) of a transmission line.

Strategy: Employ the freq. domain results that we already know.

Then take inverse Fourier transform to convert to time domain.

output impedance of signal gen.



Track changes in volt. from \hat{V}_g to $\hat{V}(-l)$:

$$\hat{V}_g - \underbrace{\hat{I}(-l)}_{\text{use } \otimes} Z_g = \underbrace{\hat{V}(-l)}_{\text{use } \oplus}$$

$$\beta = \frac{\omega}{v}$$

speed of signal

$$\hat{V}_g - \frac{V_+}{Z_0} \left[e^{j\omega l/v} - \Gamma e^{-j\omega l/v} \right] Z_g = V_+ \left[e^{j\omega l/v} + \Gamma e^{-j\omega l/v} \right]$$

solve for V_+ . We can control all other parameters using signal gen. and/or through our choice of trans. line.

$$\therefore V_+ = \frac{\hat{V}_g}{\left(e^{j\omega l/v} + \Gamma e^{-j\omega l/v} \right) + \frac{Z_g}{Z_0} \left(e^{j\omega l/v} - \Gamma e^{-j\omega l/v} \right)}$$

Assume that we chose $Z_g = Z_0$ s.t. $\frac{Z_g}{Z_0} = 1$
(typical)

$$V_+ = \frac{\hat{V}_g}{2 e^{j\omega l/s}} = \frac{\hat{V}_g}{2} e^{-j\omega l/s}$$

$$Z_0 = \sqrt{\frac{Ll}{Ce}}$$

For this case ($Z_g = Z_0$), the volt. at the trans. line input in the freq. domain is

$$\hat{U}_{in} = \hat{V}(-l) \quad \text{Eq. \# w/ } z = -l.$$

$$\hat{U}_{in} = V_+ \left[e^{j\omega l/s} + \Gamma e^{-j\omega l/s} \right]$$

$$\frac{\hat{V}_g}{2} \left[1 + \Gamma e^{-2j\omega l/s} \right] \quad \text{!}$$

Suppose we meas. the volt. at trans. line input $V_{in}(t)$ w/ an oscilloscope. We expect to meas. the inverse Fourier trans. of \hat{U}_{in} .

$$V_{in}(t) = F^{-1} \left[\hat{U}_{in}(\omega) \right]$$

$$\begin{aligned}
 v_{in}(t) &= F^{-1} \left[\frac{\hat{V}_g}{2} (1 + \Gamma e^{-2j\omega l/s}) \right] \\
 &= \underbrace{\frac{1}{2} F^{-1} [\hat{V}_g]}_{V_g(t)} + \underbrace{\frac{1}{2} F^{-1} [\hat{V}_g \Gamma e^{-2j\omega l/s}]}_I
 \end{aligned}$$

↗ signal generator output in time domain

Let's assume that Γ has no freq dependence.
 Equiv. to assuming that Z_L is just a resistor
 (not inductor or cap.)

$$I = \Gamma F^{-1} \left[\underbrace{(\hat{V}_g)}_{\hat{x}_1} \underbrace{(e^{-2j\omega l/s})}_{\hat{x}_2} \right]$$

using convolution theorem; find:

$$I = \mathcal{F}^{-1} (x_1 * x_2) (t)$$

$$= \mathcal{F}^{-1} \left(F^{-1}(\hat{x}_1) * F^{-1}(\hat{x}_2) \right) (t)$$

$$= \mathcal{F}^{-1} \left(\underbrace{F^{-1}(\hat{U}_g)}_{U_g(t)} * F^{-1}(e^{-2j\omega l/s}) \right) (t)$$

$U_g(t)$

Deal with $F^{-1}(e^{-2j\omega l/s})$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{-2j\omega l/s} e^{j\omega t} dt$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{j\omega(t - \underbrace{2l/s}_{t_0})} dt = \delta(t - t_0)$$

$$\therefore I = \mathcal{F}^{-1} \left(U_g(t) * \delta(t - t_0) \right) (t)$$

$$= \Gamma \int_{-\infty}^{\infty} V_g(\tau) \delta[(t-t_0) - \tau] d\tau$$

Recall $\int f(t) \delta(t-a) dt = f(a)$

δ -fcn selects t s.t.
 $t-a=0 \quad \therefore t=a$

δ -fcn select τ s.t. $(t-t_0) - \tau = 0$
 $\therefore \tau = t - t_0$

$$\therefore I = \Gamma V_g(t-t_0) = \Gamma V_g(t - 2l/s)$$

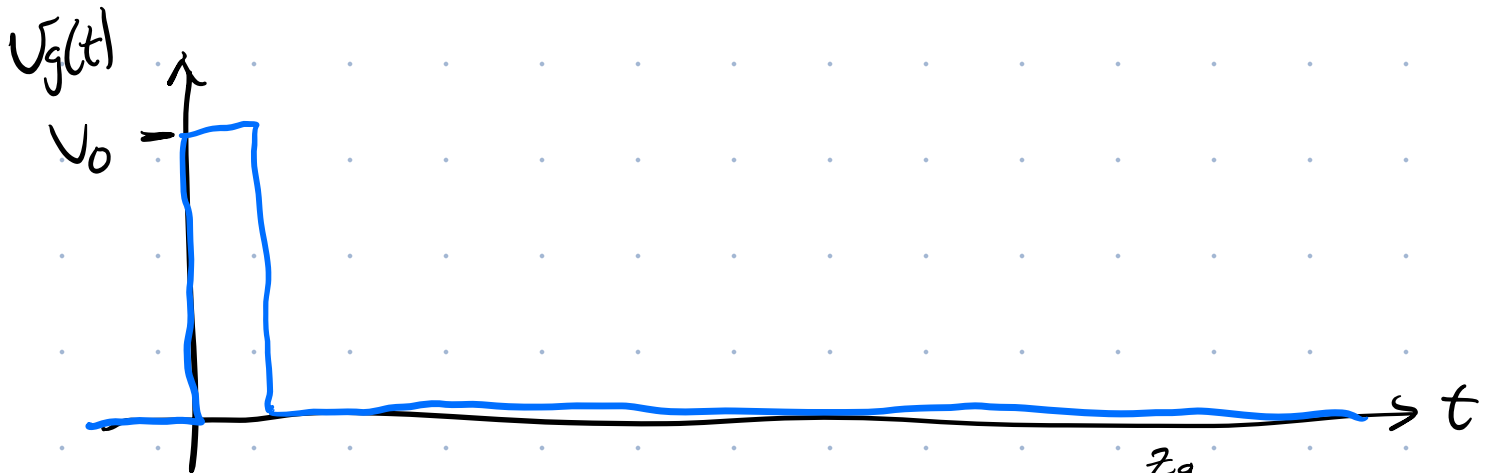
copy of fcn gen.
output delayed in
time by an amount
 $2l/s$.

Return to

$$V_{in}(t) = \frac{1}{2} V_g(t) + \frac{1}{2} \Gamma V_g(t - 2l/s)$$

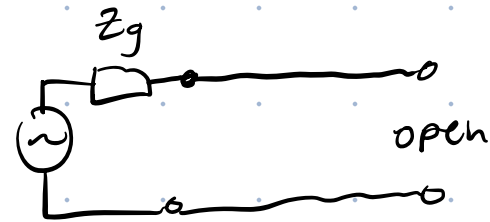
Interpret this result:

Suppose $V_g(t)$ is a square pulse



Case ①

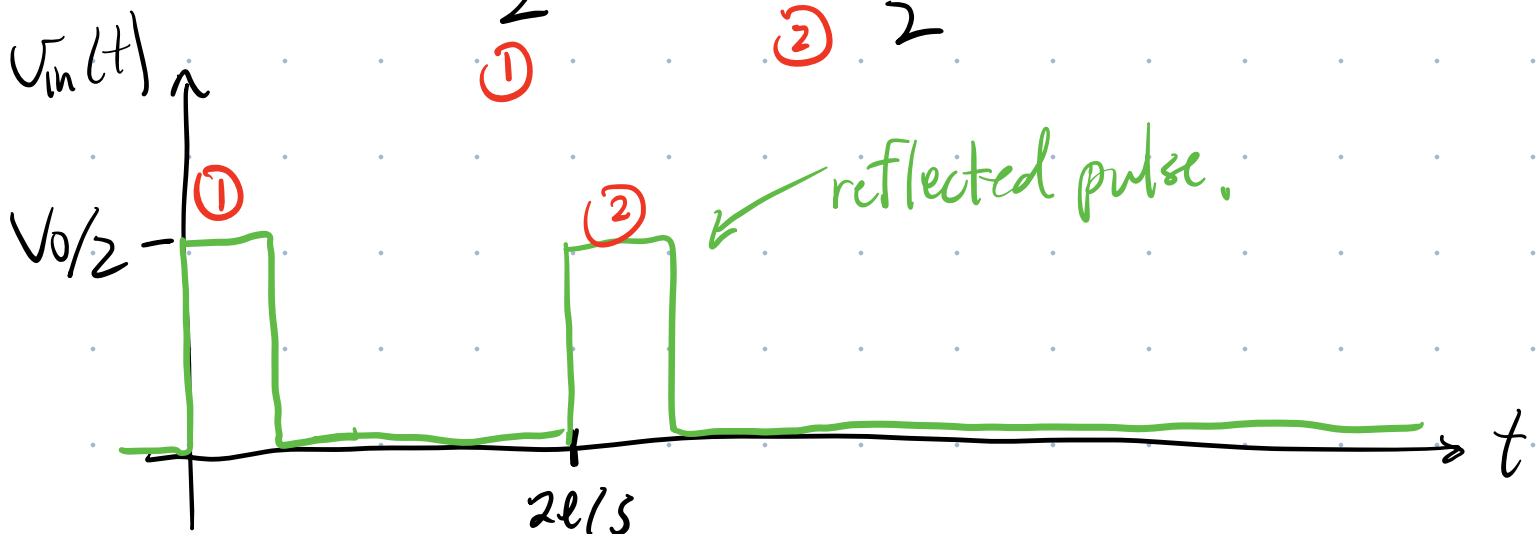
$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$$



$$Z_L \rightarrow \infty \quad (\text{open circuit})$$

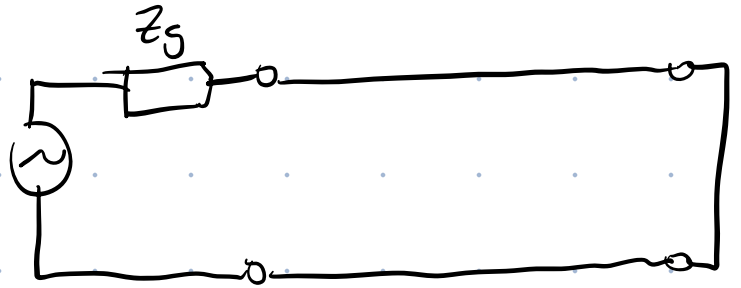
$$\Gamma = 1$$

$$V_{in}(t) = \underbrace{\frac{V_g(t)}{2}}_{\text{①}} + \underbrace{\frac{V_g(t - 2l/s)}{2}}_{\text{②}}$$

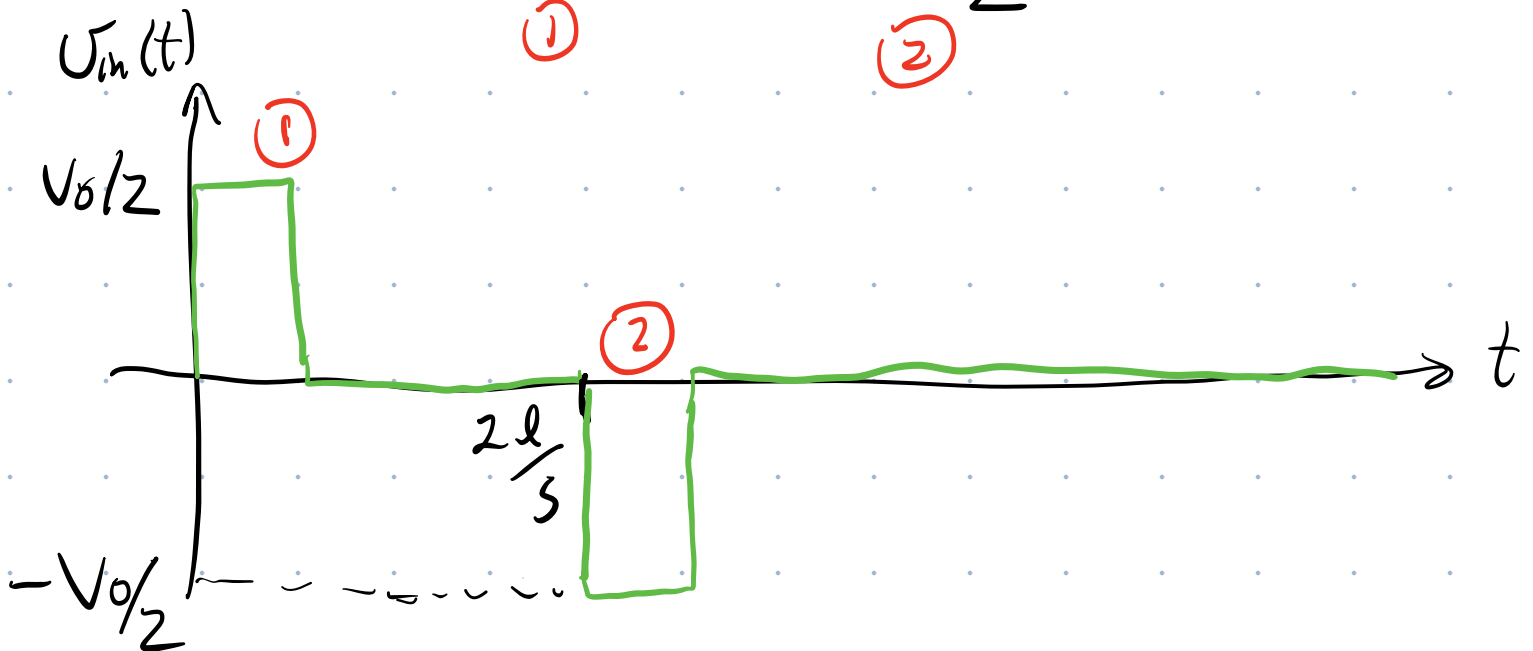


Case ② $Z_L = 0$ (short circuit)

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = -1$$

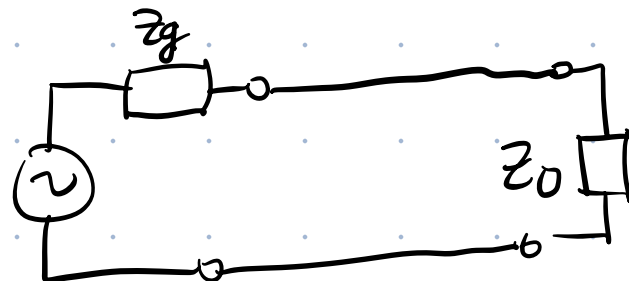


$$U_{in}(t) = \frac{U_g(t)}{2} - \frac{U_g(t - 2l/s)}{2}$$



Case ③ $Z_L = Z_0$ (50Ω)

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = 0$$



Here
$$U_{in}(t) = \frac{U_g(t)}{2}$$

