

Last Time:

Continuity Eq'n:  $\vec{\nabla} \cdot \vec{J} = -\frac{d\rho}{dt}$

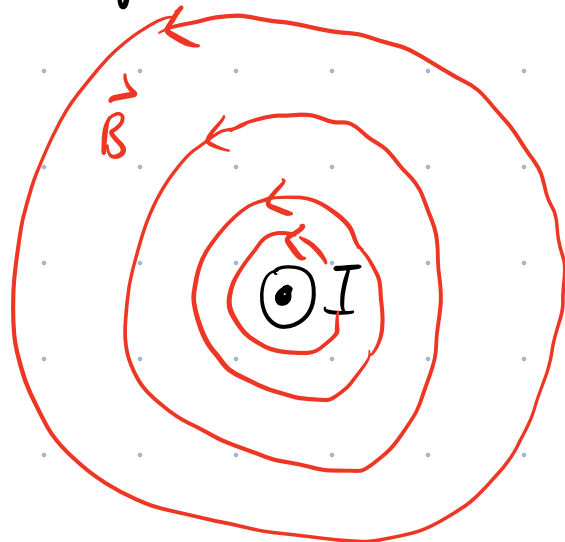
For steady currents,  $\frac{d\rho}{dt} = 0 \Rightarrow \vec{\nabla} \cdot \vec{J} = 0$

Biot-Savart Law:

$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{I} \times \hat{r}}{r^2} dl'$$

Magnetic field due to a long, straight current:

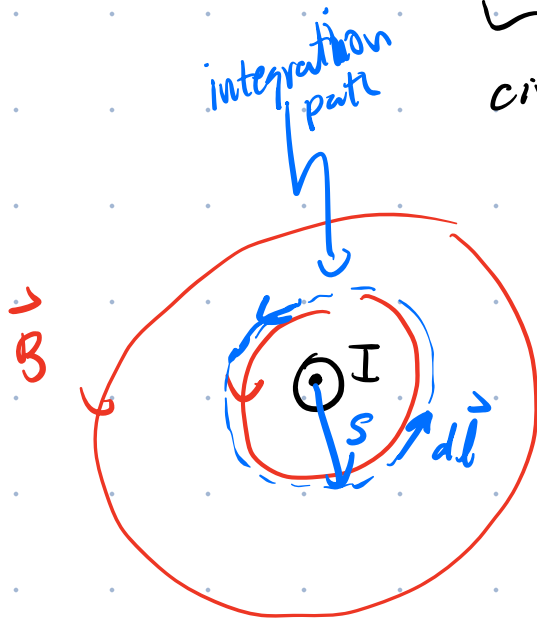
$$\vec{B} = \frac{\mu_0 I}{2\pi s} \hat{\phi}$$



# Today: Griffiths 5.3 The Divergence & Curl of $\vec{B}$

Let's try evaluating  $\oint \vec{B} \cdot d\vec{l} = \int_S \nabla \times \vec{B} \cdot d\vec{a}$

$\underbrace{\qquad\qquad\qquad}_{\text{circulation}} \qquad S \qquad \text{Stoke's Th.}$



Select an integration path that matches the symmetry of  $\vec{B}$ .

$$\therefore d\vec{l} = dl \hat{\phi} \qquad \vec{B} = \frac{\mu_0 I}{2\pi s} \hat{\phi}$$

$$\therefore \vec{B} \cdot d\vec{l} = \frac{\mu_0 I}{2\pi s} dl$$

const. on  
chosen integration path.

$$\oint \vec{B} \cdot d\vec{l} = \oint \frac{\mu_0 I}{2\pi s} dl = \frac{\mu_0 I}{2\pi s} \underbrace{\oint dl}_{\text{circumference of integration path}}$$

Integral form of Ampère's Law.

$$\therefore \oint \vec{B} \cdot d\vec{\ell} = \mu_0 I$$

$$= 2\pi r I$$

apply Stokes's Law

So far, we've shown that this result is true for a long straight current. We want generalize for  $\vec{B}$  due to any steady current dist'n.

Note that, last time we showed

$$\int_S \vec{J} \cdot d\vec{a} = I$$

$$\int_S \underbrace{\vec{\nabla} \times \vec{B}} \cdot d\vec{a} = \int_S \underbrace{(\mu_0 \vec{J})} \cdot d\vec{a}$$

must be equal

$$\therefore \vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

differential form of Ampère's Law.

#

The goal is to reproduce  $\textcircled{\#}$  starting from the general Biot-Savart Law:

$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int_V \frac{\vec{J}(\vec{r}') \times \hat{\Omega}}{\Omega^2} d\tau'$$

Integrate over primed coords which locate the source currents w.r.t. the origin. Want to find  $\vec{\nabla} \times \vec{B}$  &  $\vec{\nabla} \cdot \vec{B}$ . The  $\vec{\nabla}$  operator takes deriv. w.r.t. unprimed coords. which locate the field pt.

$$\text{Start w/ } \vec{\nabla} \cdot \vec{B} = \vec{\nabla} \cdot \left( \frac{\mu_0}{4\pi} \int_V \frac{\vec{J}(\vec{r}') \times \hat{\Omega}}{\Omega^2} d\tau' \right)$$

$$= \frac{\mu_0}{4\pi} \int_V \vec{\nabla} \cdot \left( \vec{J}(\vec{r}') \times \left( \frac{\hat{\Omega}}{\Omega^2} \right) \right) d\tau'$$

Apply product rule (6)  
from Griffiths cover

$$\frac{\hat{\rho}}{r^2} \cdot \left( \vec{\nabla} \times \vec{J}(r') \right) - \vec{J}(r') \cdot \left( \vec{\nabla} \times \frac{\hat{\rho}}{r^2} \right)$$

since deriv. w.r.t.  
unprimed coords

$$\text{since } \frac{\hat{\rho}}{r^2} = \frac{\rho}{r^3}$$

has no  $\theta$  or  $\phi$  dependence  
and no  $\theta$  or  $\phi$  component  
in spherical coords.

$$\therefore \nabla \cdot \vec{B} = 0$$

True  $\forall \vec{B}$  due to  
steady currents.

Next, consider  $\vec{\nabla} \times \vec{B}$ :

$$\vec{\nabla} \times \vec{B} = \frac{\mu_0}{4\pi} \int \vec{\nabla} \times \left( \vec{J}(\vec{r}') \times \frac{\hat{r}}{r^2} \right) d\tau'$$

Product rule  
(8)

$$\begin{aligned} & \left( \frac{\hat{r}}{r^2} \cdot \vec{\nabla} \right) \vec{J}(\vec{r}') - \left( \vec{J}(\vec{r}') \cdot \vec{\nabla} \right) \frac{\hat{r}}{r^2} \\ & + \vec{J}(\vec{r}') \left( \vec{\nabla} \cdot \frac{\hat{r}}{r^2} \right) - \frac{\hat{r}}{r^2} \left( \vec{\nabla} \cdot \vec{J}(\vec{r}') \right) \end{aligned}$$

$4\pi \delta^3(\vec{r})$

$$\vec{\nabla} \times \vec{B} = \mu_0 \int \vec{J}(\vec{r}') \delta^3(\vec{r} - \vec{r}') d\tau'$$

$$- \frac{\mu_0}{4\pi} \int \left( \vec{J}(\vec{r}') \cdot \vec{\nabla} \right) \frac{\hat{r}}{r^2} d\tau'$$

$\text{Int}_2$

selects  
value of  $\vec{r}'$   
s.t.  $\vec{r} - \vec{r}' = 0$   
 $\Rightarrow \vec{r} = \vec{r}'$

We will show that  $\text{Int}_2 = 0$  s.t.

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

Aside: Consider  $\frac{\partial}{\partial x} f(u)$  where  $u = x - x'$

$$= \frac{df}{du} \frac{du}{dx} = \frac{df}{du}$$

Consider  $\frac{\partial}{\partial x'} f(u)$

$$= \frac{df}{du} \frac{du}{dx'} = - \frac{df}{du}$$

$$\frac{\partial}{\partial x'} f(u) = - \frac{\partial}{\partial x} f(u)$$

By the same logic,  $\vec{\nabla} \frac{\hat{r}}{r^2}$  in  $\text{Int}_2$   
is equiv. to  $-\vec{\nabla}' \frac{\hat{r}}{r^2}$

$\therefore$  Int<sub>2</sub> becomes:

$$-\frac{\mu_0}{4\pi} \int \left( \vec{J}(\vec{r}') \cdot \vec{\nabla}' \right) \frac{1}{r^2} d\tau'$$

Consider just the x-comp. of  $\frac{1}{r^2}$  is Cartesian coord.

$$\frac{1}{r^2} = \frac{x}{r^3}$$

$$\left( \vec{J}(\vec{r}') \cdot \vec{\nabla}' \right) \left( \frac{x-x'}{r^3} \right)$$

Product rule  
(5)

$$= \vec{\nabla}' \cdot \left( \frac{x-x'}{r^3} \vec{J}(\vec{r}') \right)$$

$$- \left( \frac{x-x'}{r^3} \right) \underbrace{\vec{\nabla}' \cdot \vec{J}(\vec{r}')}$$

0 for steady currents

(continuity eq'n w/  
 $\frac{d\rho}{dt} = 0$ )



∴ the x-component's contribution to  $\text{Int}_2$  is

$$\int_V \vec{\nabla}' \cdot \left( \frac{x-x'}{r^3} \vec{J}(\vec{r}') \right) d\tau'$$

Apply the divergence theorem

$$= \oint_S \frac{x-x'}{r^3} \vec{J}(\vec{r}') \cdot d\vec{a}'$$

$S \leftarrow$  surface bounding the integral in Biot-Savart law that contains  $\vec{J}(\vec{r}')$ .

Choose surface to be large enough that  $\vec{J}(\vec{r}') = 0$  everywhere on the surface  $S$ .

$\text{Int}_2 = 0$ . (similar for y & z components).

Summary

Ampère's Law  
in differential  
form

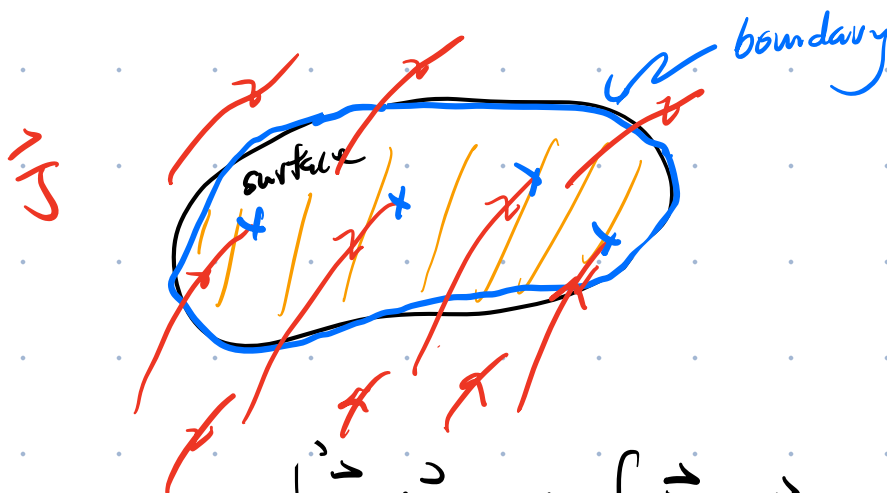
$$\vec{\nabla} \cdot \vec{B} = 0$$
$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

valid  $\forall$  magneto-  
statics.

### 5.3.3 Ampère's Law

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

Integrate  $\int_S \vec{\nabla} \times \vec{B} \cdot d\vec{a} = \oint_{\text{boundary}} \vec{B} \cdot d\vec{l}$

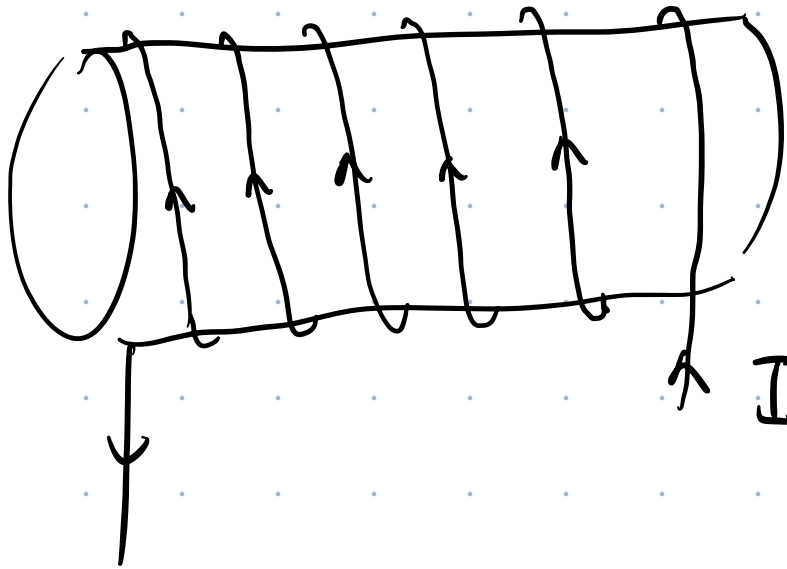


$$\oint \vec{B} \cdot d\vec{l} = \mu_0 \int \vec{J} \cdot d\vec{a} = \mu_0 I$$

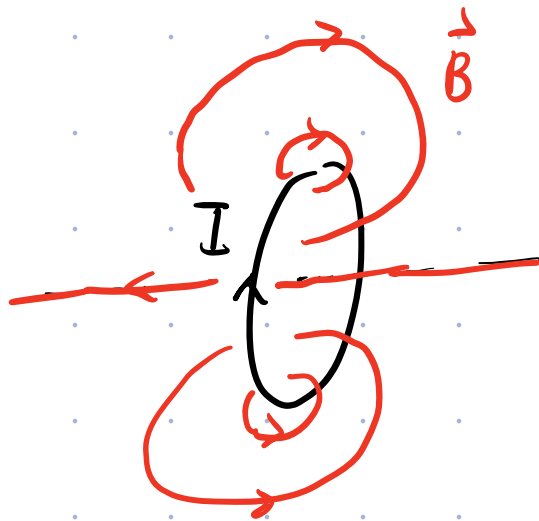
$I_{\text{encl}}$  ← total current passing surface  $S$ .

$$\therefore \oint \vec{B} \cdot d\vec{l} = \mu_0 I_{\text{encl}} \quad \text{integral form of Ampère's Law}$$

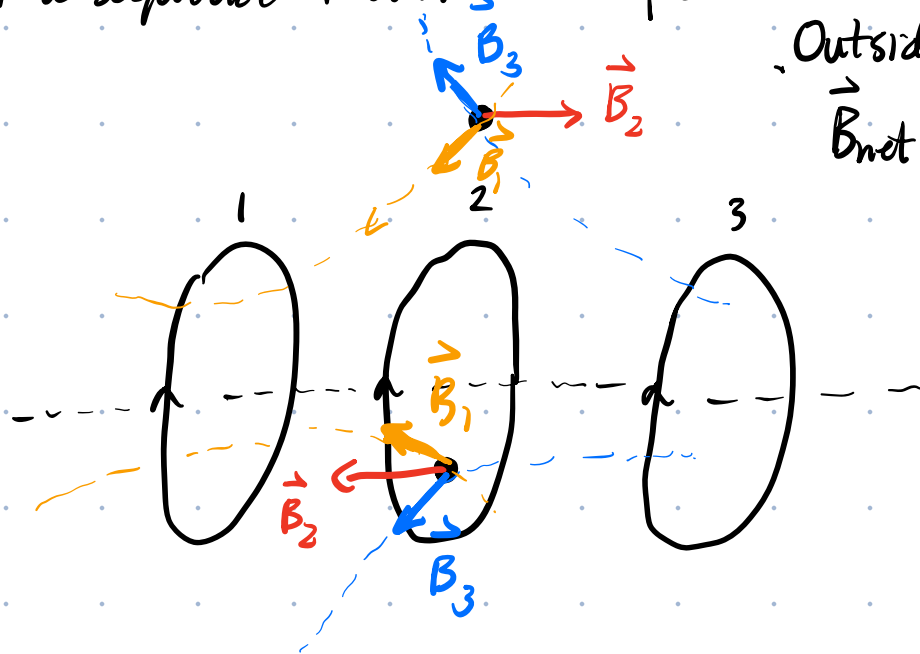
Ex. Find  $\vec{B}$  due to a long solenoid.



Like a series of current loops.



Consider a sequence of current loops

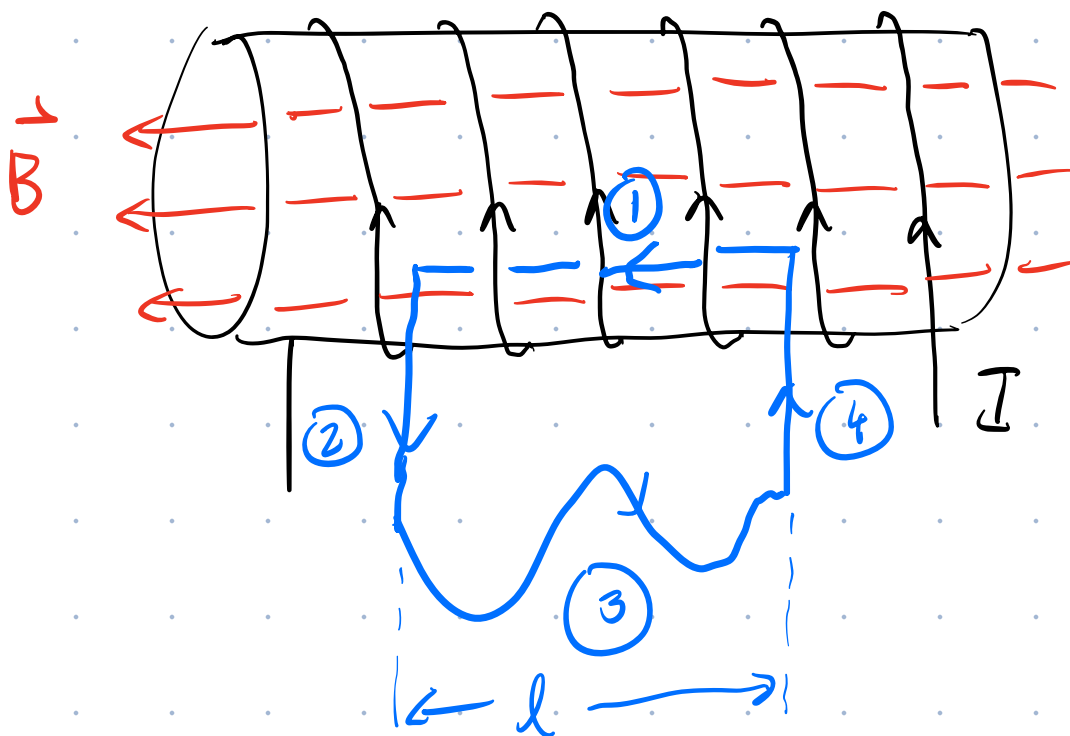


Outside the solenoid  
 $\vec{B}_{net} \approx 0$

Inside solenoid, horizontal  $\vec{B}$ -field is strong while the vertical component vanishes

Apply Ampère's to the solenoid

$$B = 0$$



1. Select an Amperian loop/integration path

path: - should be  $\parallel$  or  $\perp$  to  $\vec{B}$

-  $B$  should be const. when path  $\parallel$  to  $\vec{B}$ .

2. Find  $I_{\text{enc}}$  (how much current passes through Amperian loop)

$N$  loops of the solenoid coil pass through the loop.

$$\therefore I_{\text{enc}} = NI$$

3. Evaluate  $\oint \vec{B} \cdot d\vec{l} = \int_{\textcircled{1}} \vec{B} \cdot d\vec{l} + \int_{\textcircled{2}} \vec{B} \cdot d\vec{l}$

$$+ \int_{\textcircled{3}} \vec{B} \cdot d\vec{l} + \int_{\textcircled{4}} \vec{B} \cdot d\vec{l}$$

0 b/c  $\vec{B} \perp d\vec{l}$  inside solenoid  
 $\vec{B} = 0$  outside solenoid.

0 b/c  $\vec{B} = 0$  everywhere on  $\textcircled{3}$   
0 for same reasons as  $\textcircled{2}$

$$\oint \vec{B} \cdot d\vec{\ell} = \int_{\textcircled{1}} \vec{B} \cdot d\vec{\ell} = \int B dl$$

since  $\vec{B} \parallel d\vec{\ell}$  for  $\textcircled{1}$

$$= B \int dl$$

since  $\textcircled{1}$  is same position  
inside solenoid (same dist.  
for solenoid axis)

$$= B l$$

$\uparrow$  length of path  $\textcircled{1}$

Finally:  $\oint \vec{B} \cdot d\vec{\ell} = \mu_0 I_{\text{enc}}$

$\Downarrow$

$$B l = \mu_0 N I$$

$n$ : no. of turns  
per unit length.

$$\therefore B = \mu_0 \left( \frac{N}{l} \right) I$$

$$\therefore B = \mu_0 n I$$

$\vec{B}$  inside solenoid is uniform.