

- Assignment #5 is on course website this weekend
- Start working on your formal report
  - due April 7 @ 14:00 in SCI 241

Last Time: given a linear set of data  $(x_i, y_i \pm \sigma_i)$ , the best intercept & slope for the line passing through the data are given by:

$$a = \frac{1}{\Delta} \left( \sum \frac{x_i^2}{\sigma_i^2} \sum \frac{y_i}{\sigma_i^2} - \sum \frac{x_i}{\sigma_i^2} \sum \frac{x_i y_i}{\sigma_i^2} \right)$$

intercept

$$\Delta = \sum \frac{1}{\sigma_i^2} \sum \frac{x_i^2}{\sigma_i^2} - \left( \sum \frac{x_i}{\sigma_i^2} \right)^2$$

$$\sigma_a^2 = \frac{1}{\Delta} \sum \frac{x_i^2}{\sigma_i^2}$$

$$b = \frac{1}{\Delta} \left( \sum \frac{1}{\sigma_i^2} \sum \frac{x_i y_i}{\sigma_i^2} - \sum \frac{x_i}{\sigma_i^2} \sum \frac{y_i}{\sigma_i^2} \right)$$

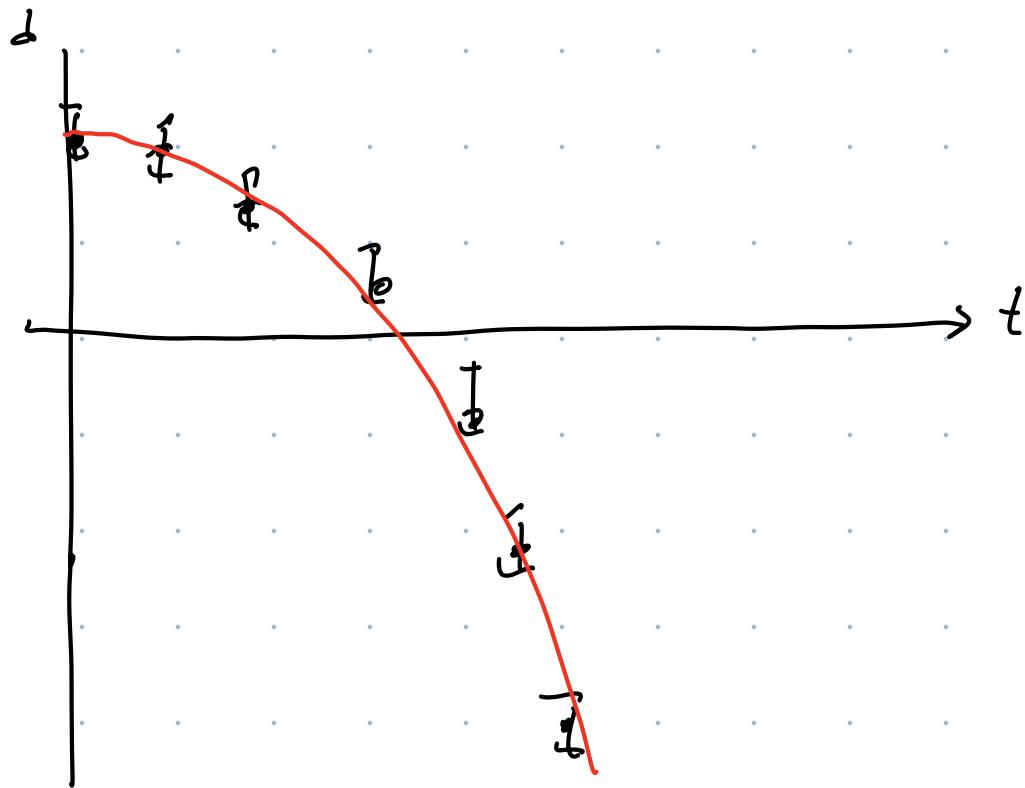
slope.

$$\sigma_b^2 = \frac{1}{\Delta} \sum \frac{1}{\sigma_i^2}$$

# Today: Linearizing data

E.g. Object in free starting rest

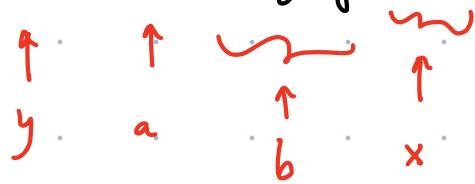
$$d = d_0 - \frac{1}{2} g t^2$$

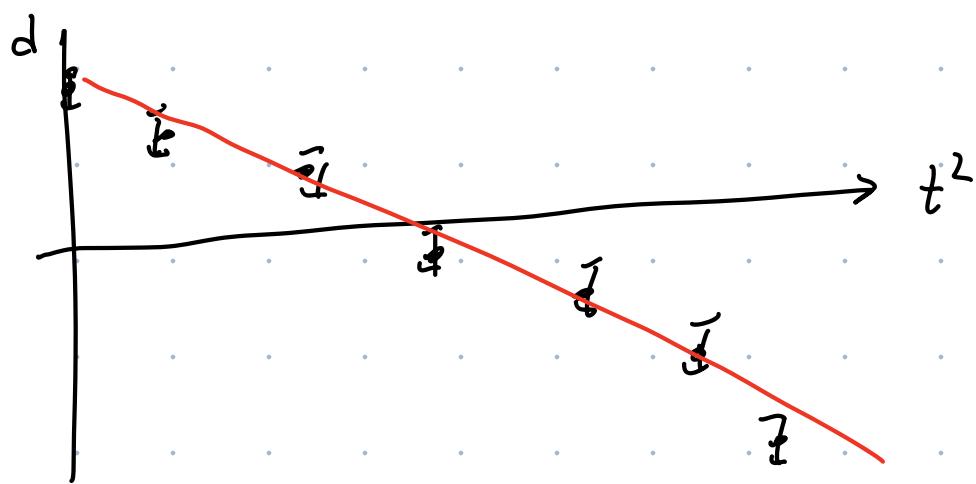


Instead of plotting  $d$  vs  $t$  consider

$d$  vs  $t^2$

$$d = d_0 - \frac{1}{2} g (t^2)$$





Another example: In thermal waves, the amplitude of the fundamental fourier component is

$$A_1 = \left( \frac{4T_0}{\pi} \right) \exp \left( - \sqrt{\frac{\omega}{2\alpha}} x \right)$$

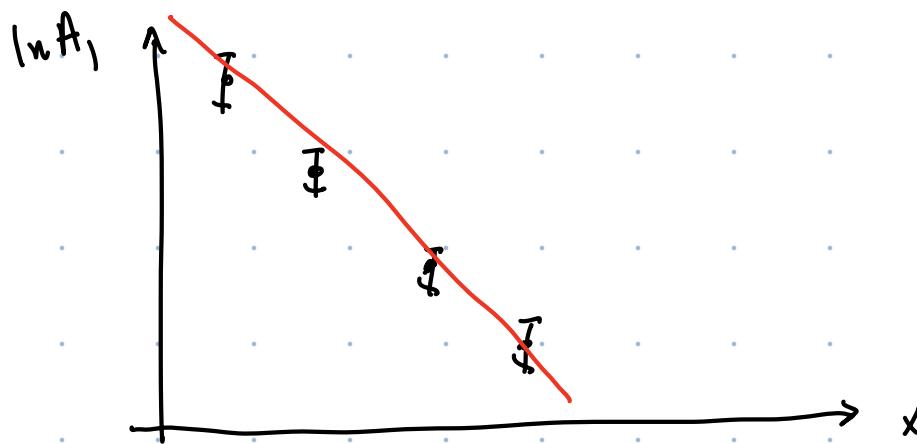
To linearize, take the ln of both sides

$$\ln A_1 = \ln \left( \frac{4T_0}{\pi} \right) + \left( - \sqrt{\frac{\omega}{2\alpha}} \right) x$$

y      a      x  
b

slope  $b$  is related to the thermal diffusivity  $\alpha$ .

$$b^2 = \frac{\omega}{2\alpha} \Rightarrow \boxed{\alpha = \frac{\omega}{2b^2}}$$



Another example (used in current research)

Low-temperature thermal conductivity of a conductor is typically of the form:

$$K = \underbrace{C_1 T}_{\text{electron contribution}} + \underbrace{C_3 T^3}_{\text{lattice/phonon contribution}}$$

Meas. K as a fn of T. Does not appear to be easily linearized at first glance.

Consider  $\frac{K}{T} = C_1 + C_3 T^2$

$\downarrow$	$\downarrow$	$\downarrow$	$\downarrow$
$y$	$a$	$b$	$x$

Plot  $\frac{K}{T}$  vs  $T^2$ , get intercept  
slope

$$\begin{aligned} a &= C_1 \\ b &= C_3 \end{aligned}$$

Another example: Sometimes a pair of variables cannot be strictly linearized.

In Blackbody radiation

$$I = \frac{2c^2 h}{\lambda^5} \left[ \frac{1}{e^{hc/\lambda k_B T} - 1} \right]$$

meas  $I$  vs  $T$ , its not linear.

However, under certain conditions, can make valid approx. that allow the data to be linearized.

In this case, if  $\frac{hc}{\lambda k_B T} \gg 1$

$$\text{then } e^{hc/\lambda k_B T} - 1 \approx e^{hc/\lambda k_B T}$$

$$\therefore I \approx \frac{2c^2 h}{\lambda^5} e^{-hc/\lambda k_B T}$$

Now, we can take the ln of both sides:

$$\ln I = \ln \left( \frac{2c^2 h}{\lambda^5} \right) + \left( -\frac{hc}{\lambda k_B} \right) \frac{1}{T}$$

y
a
b
x

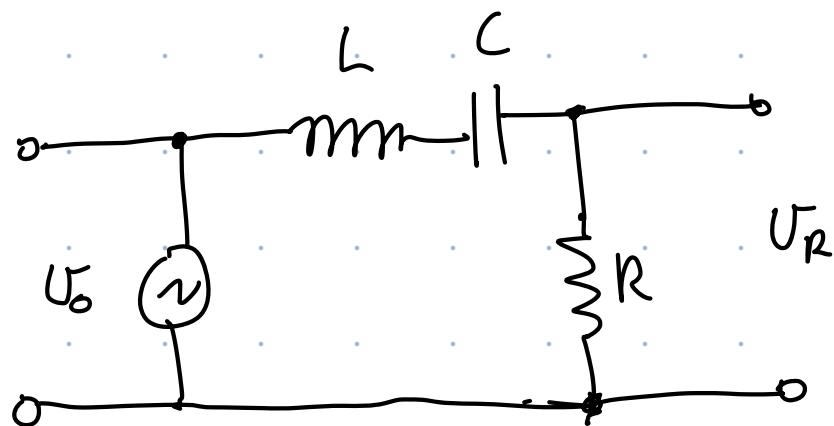
$$\Rightarrow b = -\frac{hc}{\lambda k_B}$$

i:

$$h = -\frac{\lambda k_B b}{c}$$

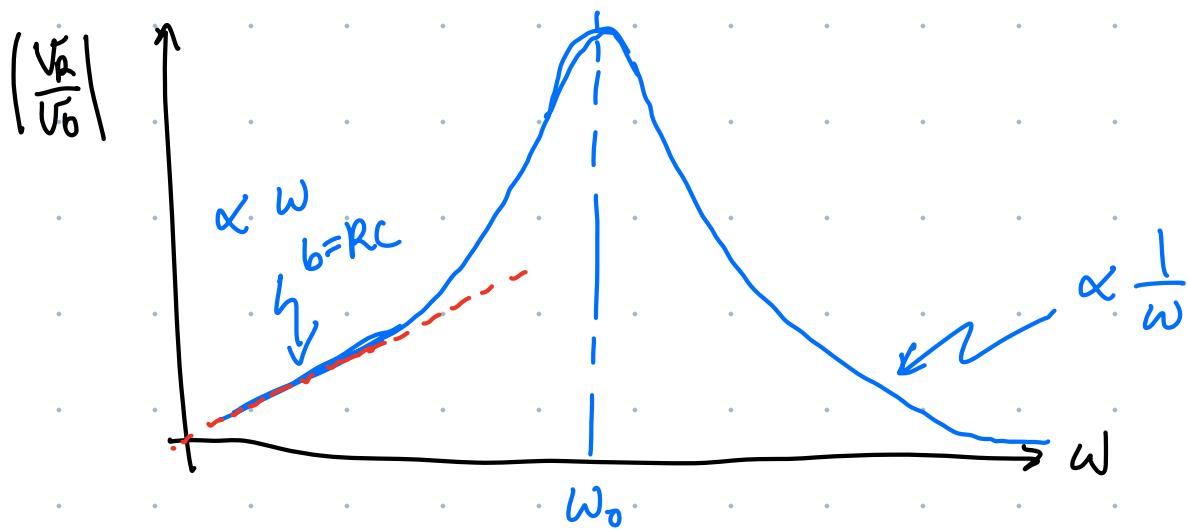
Sometimes it's just not possible to linearize a data set.

Eg. LRC resonance



meas.  $\left| \frac{U_R}{U_0} \right|$  vs  $\omega$

$$\left| \frac{U_R}{U_0} \right| = \frac{1}{\sqrt{1 + \left( \frac{\omega L}{R} - \frac{1}{\omega RC} \right)^2}}$$



$\left| \frac{V_R}{V_0} \right|$  is clearly not linear.

Check behaviour at low freq, ( $\omega \rightarrow 0$ )

$$\left| \frac{V_R}{V_0} \right| \approx \frac{1}{\sqrt{1 + \left( -\frac{1}{\omega RC} \right)^2}} \approx \frac{1}{\frac{1}{\omega RC}} = \omega RC$$

At low freq,  $\left| \frac{V_R}{V_0} \right|$  vs  $\omega$  is linear w/  
slope  $b = RC$

Check behaviour at high freq ( $\omega \rightarrow \infty$ )

$$\left| \frac{V_R}{V_0} \right| \approx \frac{1}{\sqrt{1 + \left( \omega \frac{L}{R} \right)^2}} \approx \frac{1}{\omega \frac{L}{R}} = \left( \frac{R}{L} \right) \frac{1}{\omega}$$

At high freq, can plot  $\left| \frac{V_R}{V_0} \right|$  vs  $\frac{1}{\omega}$  to find a  
slope  $b = \frac{R}{L}$

Can we fit the entire freq. dependence?

start w/

$$\left| \frac{V_R}{V_0} \right| = \frac{1}{\sqrt{1 + \left( \omega \frac{L}{R} - \frac{1}{\omega RC} \right)^2}}$$

Square both sides...

$$\left| \frac{V_R}{V_0} \right|^2 = \frac{1}{1 + \left( \omega \frac{L}{R} - \frac{1}{\omega RC} \right)^2}$$

invert

$$\left( \frac{V_0}{V_R} \right)^2 = 1 + \left( \omega \frac{L}{R} - \frac{1}{\omega RC} \right)^2$$

expand the square

$$\left| \frac{V_0}{V_R} \right|^2 = \left( 1 - \frac{2L}{R^2 C} \right) + \omega^2 \left( \frac{L}{R} \right)^2 + \frac{1}{\omega^2 (RC)^2}$$

Not linearizable

Need some new fitting techniques for funcs that cannot be linearized.

Eg. Calibration of a thermocouple over a large span of temperatures follows a polynomial dependence.

Fitting  $T$  vs  $V$  to a polynomial

$$T = a_0 + a_1 V + a_2 V^2 \leftarrow \text{not linearizable.}$$

In general, we want to be able to fit data to a fn of the form:

$$y(x) = a_0 + a_1 x + a_2 x^2 + \dots + a_m x^m$$

In fact, the technique that we'll develop can be further generalized to fit data to a fn of the form:

$$y(x) = a_1 f_1(x) + a_2 f_2(x) + \dots + a_m f_m(x)$$

Here,  $f_k(x)$  are fns of  $x$  that do not involve the unknown parameters  $a_1, a_2, \dots, a_m$  that we're trying to determine.

For example, for a polynomial up to  $x^2$

$$f_1 = 1, \quad f_2 = x, \quad f_3 = x^2$$

s.t.

$$y = a_1 + a_2 x + a_3 x^2 \rightarrow \text{thermocouple example.}$$

or, for the LRC example, we can take

$$f_1 = 1, \quad f_2 = \omega^2, \quad f_3 = \frac{1}{\omega^2}$$

s.t.

$$y = a_1 + a_2 \omega^2 + a_3 \frac{1}{\omega^2}$$
$$\left(1 - \frac{2L}{RC}\right) \quad \left(\frac{L}{R}\right)^2 \quad \left(\frac{1}{RC}\right)^2$$

Next time, apply method of maximum likelihood to determine the best-fit parameters for fits to functions of the form:

$$y = a_1 f_1(x) + a_2 f_2(x) + \dots + a_m f_m(x)$$